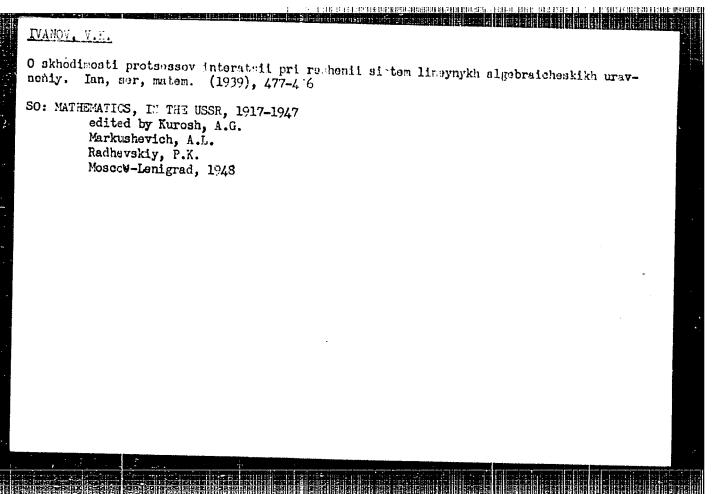
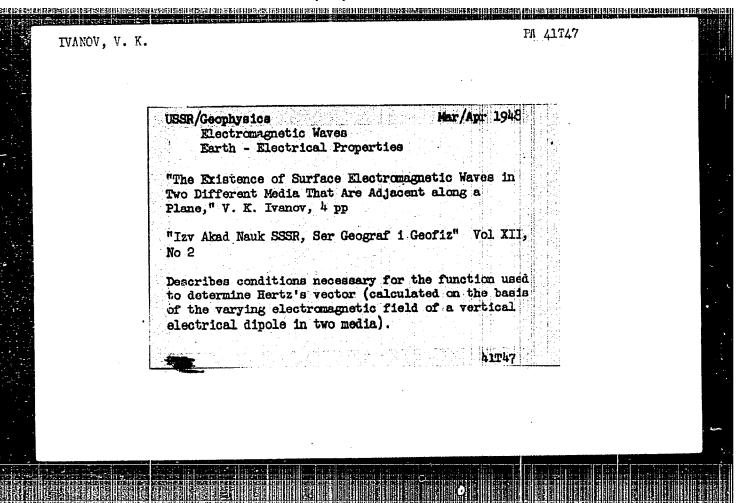
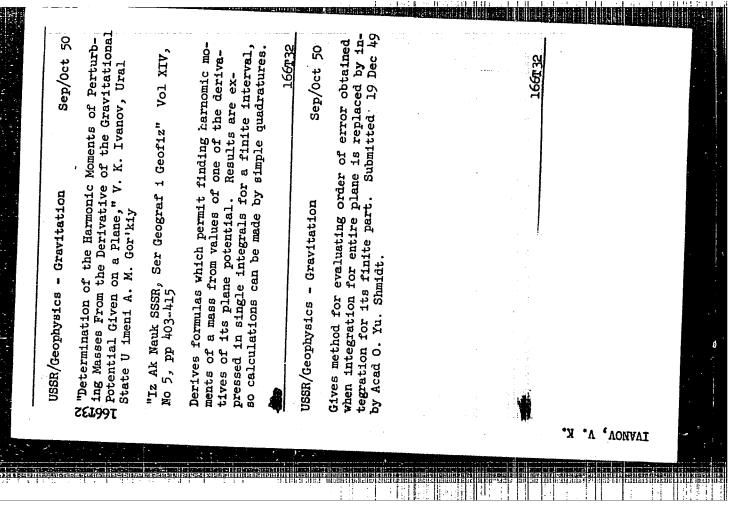


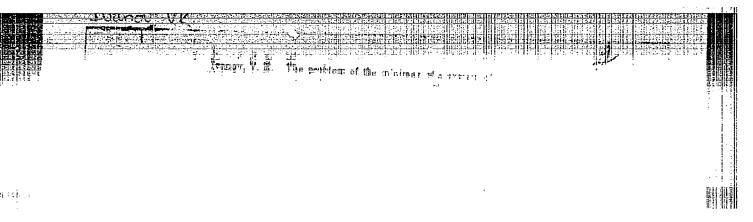
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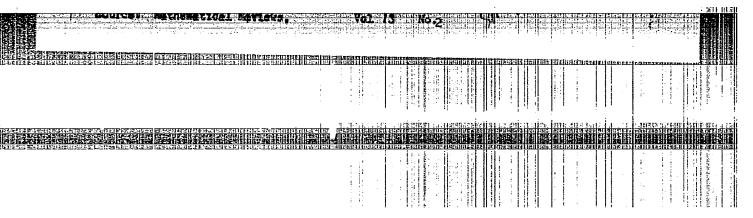


PA 23/49T70 V.K. IVANOV USSR/Mathematics - Operational Theory Nov/Dec 48 Mathematics - Transformations "Fourier's Generalized Transformation in Operational Calculus, V. K. Ivanov, Sverdlovsk, Ural State U imeni A. M. Gor'kiy, 16 pp "Matemat Shor" Vol IXIII (IXV), No 3 Author proposes construction of a theory which will permit formal operations with Fourier integrals to be effected during solution of problems in mathematical physics. He does this by unifying the basic concepts of Bochner's theory of generalized trigonometric integrals with Gunter's ideas on problems of mathematical physics. 23/49170









IVANOV, W., KU

USSR/Mathematics - Approximations, Uniform May/Jun 52

"Uniform Approximations of Continuous Functions," V. K. Ivanov, Sverdlovsk

"Matemat Sbor" Vol XXX (72), No 3, pp 543-558

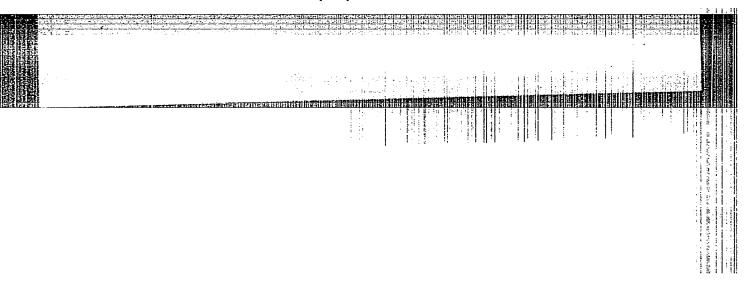
Discusses P. L. Chebyshev's problem concerning uniform approximations of a complex continuous function f(x) defined on a compact space X by complex quasi-polynomials of the form $P(x) = a_1L_1(x) + \ldots + a_nL_n(x)$, where $L_1(x)$ are complex continuous functions defined in X. Submitted 5 Jun 51.

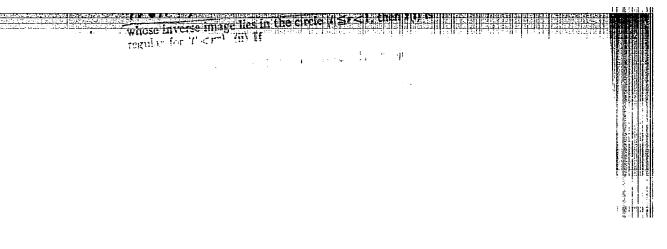
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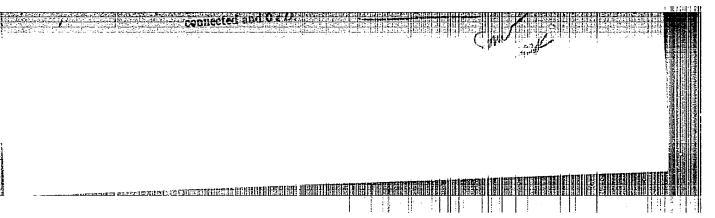
Ural State U imeni Gor'kiy, Academic degree of Doctor of Physico-Mathematical Sciences, based on his defense, 29 December 1955, in the Council of the Nathematics Inst imeni Steklov, Acad Sci USSR, of his dissertation entitled: "Investigations of the reciprocal problem of potential."

Academic degree and/or title: Doctor of Sciences

SO: Decisions of VAK, List no. 5, 3 March 56, Byulleten' MVO SSSR, No. 2, Jan 57, Moscow, pp 17-20, Uncl. JPRS/NY_466







IVANOV, V.K.

SUBJECT

CARD 1/2 PG - 553 USSR/MATHEMATICS/Theory of functions

AUTHOR

On the distribution of singularities of a potential.

Uspechi mat. Nauk 11, 5, 67-70 (1956) TITLE PERIODICAL

reviewed 1/1957

The author solves the following problem: In a halfplane y>0 finite masses are distributed which fill up a finite region D of the XY-plane. On the straight line y = 0 the derivative V of the potential is known. Determine

the distance H of the OX-axis from the set of singularities of the outer potential V at its analytic continuation into the inner of the masses. An analogous problem is considered in the space (the masses are distributed in the halpspace z > 0 and on z = 0, V_z is given). In the plane case the author obtains

$$H = -\frac{\ln |v_1(r)|}{r \to \infty}$$

where

$$v_1(r) = \int_{-\infty}^{+\infty} e^{irx} v_y(x,0) dx.$$

In the spatial case:

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Uspechi mat. Nauk 11, 5, 67-70 (1956)

CARD 2/2 PG - 553

 $H = \inf_{\varphi} \left[-\frac{1}{\lim_{r \to \infty}} \frac{\ln v_1(r \cos \varphi, r \sin \varphi)}{r} \right]$

where

 $v_1(\xi, \eta) = \frac{1}{2} \int_{e^{i(x\xi+y\eta)}}^{+\infty} v_2(x,y,0) dxdy.$

For the considerations of the spatial case the author uses ideas of Bicadze (Izvestija Akad. Nauk 17, 525-538 (1953))-

INSTITUTION: Moscow.

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IVANOV, V.K

SUBJECT

USSR/MATHEMATICS/Integral equations

PG - 569 CARD 1/2

AUTHOR

TITLE

The inverse potential problem for a body being little different

from a given body.

PERIODICAL

Izvestija Akad. Nauk 20, 793-818 (1956)

reviewed 2/1957

Let the body T be bounded by the surface S and be filled with a medium of density 1. Let S belong to the class BL according to Lichtenstein (Encykl.d. Math. Wiss. II, 3, 177-377), V be the outer potential of T. Let a harmonic function V, be defined outside of S, being regular in infinity, satisfying the

condition $\lim_{r\to\infty} v_1 \cdot r > 0$ and being continuable over S into the inner of T. The limit values of the derivatives $\frac{\partial v}{\partial v}$, $\frac{\partial^2 v}{\partial v^2}$, $\frac{\partial^2 v}{\partial v}$, $\frac{\partial^2 v}{\partial v^2}$ with respect to

the outer normal are functions of the space R2 on S (Lichtenstein: Lectures on some classes of non-linear integral equations, p. 123). Under the assumption that the norms

$$\left\| \Lambda^{1} - \Lambda \right\| , \left\| \frac{9 \Lambda}{3 \Lambda^{1}} - \frac{9 \Lambda}{9 \Lambda} \right\| , \left\| \frac{9 \Lambda_{5}}{9_{5} \Lambda^{1}} - \frac{9 \Lambda_{5}}{9_{5} \Lambda} \right\|$$

are sufficiently small, the author seeks the body T_1 which is bounded by S_1 and

Izvestija Akad. Nauk 20, 793-818 (1956)

CARD 2/2

PG - 569

and posesses the outer potential V_1 .

The author proves not only the existence and uniqueness of the solution but moreover he shows that the solution can be obtained constructively by successive approximation. The starting point is the set up of an integrodifferential equation in curvilinear coordinates for the sought surface S₁.

Then it is proved that every sufficiently small solution of the integrodifferential equation is a solution of the problem in question. The convergence of the successive approximation is proved by aid of the differentiable derivatives of Lichtenstein. The present investigations base on the papers of Lichtenstein.

"APPROVED FOR RELEASE: 03/20/2001

CIA-RDP86-00513R000619130003-8

IVANOV , V.K.

PG - 617 CARD 1/2 USSR/MATHEMATICS/Functional analysis SUBJECT

AUTHOR

The distribution of singularities of a potential and a spatial TITLE

analogue of the theorem of Polya.

Mat.Sbornik, n. Ser. 40, 319-338 (1956) PERIODICAL

reviewed 2/1957

Let a mass be distributed in the finite region D which lies in the Hilbert space z > 0 (or in the half plane y > 0). The outer potential V of this mass can be continued with respect to D as a harmonic function. The distance H from the plane z = 0 (or from the straight line y = 0) to the set of singularities of the obtained harmonic function shall be determined. Let be given the derivative V_z (or V_y) of the potential in the plane z=0 (or on the straight line y = 0). In the two-dimensional case the author finds:

(1)
$$H = -\frac{\lim}{r \to \infty} \frac{\log |v_1(r)|}{r}$$
, $v_1(r) = \int_{-\infty}^{+\infty} e^{irx} v_y(x,0) dx$

and in the three-dimensional case:

and in the three-dimensional case:

(2)
$$H = -\sup_{\psi} \frac{1}{1 \text{ im}} \frac{\log |v_1(r \cos \psi, r \sin \psi)|}{r}$$
, $v_1(\xi, \gamma) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{i(x\xi + y \chi)} v_2(x, y, 0) dx dy$

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Mat.Sbornik, n. Ser. 40, 319-338 (1956)

CARD 2/2

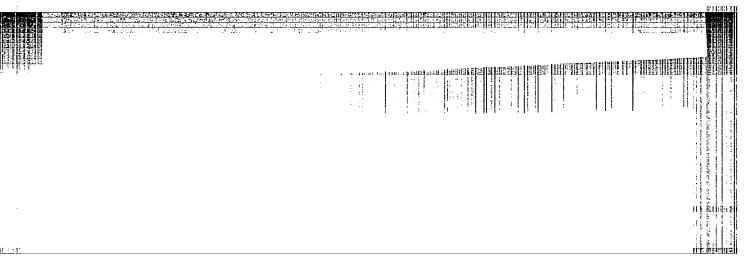
PG - 617

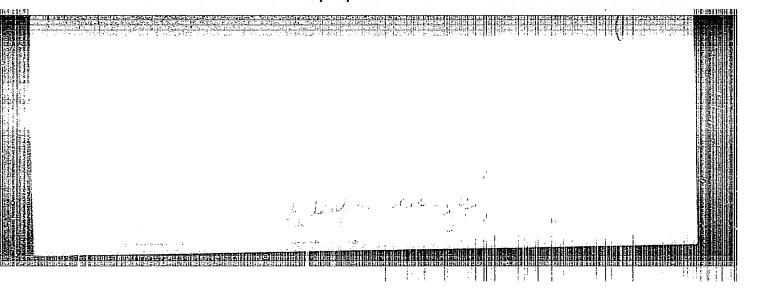
(1) is obtained by aid of Laplace's curve integrals and a theorem on entire functions of Polya (Math.Z. 29, 549-600). In the spatial case the author uses the potential-harmonic vector functions instead of analytic functions and thereby all is reduced to the two-dimensional scheme. It is shown that (2) is connected with the following generalization of a theorem of Polya: Let V be the outer potential of a finite mass which fills up a bounded region. Let $K_1(\theta, \varphi)$ be the support function of the convex closure of the set of singularities of V at a continuation of V into the interior of the considered region. Let $h_1(\Psi, \theta, \varphi)$ be the indicatrix of the increase of the characteristic distribution function of the masses. Then the equation

$$K_1(\theta, \varphi) = \sup_{\psi} h_1(\psi, \theta, \psi + \frac{\pi}{2})$$

is valid.

INSTITUTION: Sverdlovsk.





39-3-5/8 IVAHOV, V.K. (Sverdlovsk) Connection Between the Increase of an Entire Function of AUTHOR: many Variables and the Distribution of the Singularities of TITLE: Its Associated Function (Svyaz' mezhdu rostom tseloy funktsii mnogikh peremennykh i raspremelentyem osobennostey assotsiirovannoy s ney funktsii) Matematicheskiy Sbornik, 1957, Vol. 43, Nr 3, pp. 367-378 (USSR) PERIODICAL: According to Polya's theorem it is ABSTRACT: p (4) = K (-1) where h(4) is the indecatrix of increase of the function $F(z) = \sum_{n=0}^{\infty} \frac{a_n}{n!} z^n$ and K(P) is the supporting function of n=0 the convex envelope of the singularities of $f(z) = \sum_{n=0}^{\infty} \frac{a_n}{n+1}$. The author transfers this statement to functions of several variables as follows: If in the z-plane the straight line $\Gamma(\P)$ which forms the angle f with the real axis is drawn and if on it the semi-infinite intervals B(f) and S(f) are defined by the conditions $OP_1 > E(f)$, $P_1 : B(f)$ and $OP_2 : h(f)$, Card 1/3

APPROVED FOR RELEASE: 03/20/2001

CIA-RDP86-00513R000619130003-8"

39-3-5/8

Connection Between the Increase of an Entire Function of Meny Variables and the Distribution of the Singularities of Its Associated Function

 $P_2 \in S$ (4), then (1) is equivalent to the relation $\bar{B}(-\phi) = \bar{S}(\phi)$. (1) expresses that the limits of the domains B (- φ) and S (φ)

now be $F(z_1, \dots, z_n) = \underbrace{ \frac{a_{m_1, m_2, \dots, m_n}}{m_1! \dots m_n!}} \frac{a_{m_1, \dots, m_n}}{a_1! \dots a_n!} z_1^{m_1 \dots a_n}$ are identical. Let now be

and let the associated function be

 $f(z_1, \dots, z_n) = \frac{m_1 \cdots m_n}{m_1 + 1 \dots m_{n+1}}$

Let through the origin of the 2n-dimensional space of the complex variable: z_1, \dots, z_n an oriented n-dimensional plane $\Gamma\left(\begin{smallmatrix}0\\1\end{smallmatrix},\cdots\begin{smallmatrix}\rho\\n\end{smallmatrix}\right)$ be laid which is determined by the arguments z_1, \dots, z_n of the variables z_1, \dots, z_n . On this plane the author constructs the domains B $(\gamma_1, \dots, \gamma_n)$ and $S(\gamma_1, \dots, \gamma_n)$ whereby B is defined by the distribution of the singularities of f and 5 by the increase of F . Now it is proved that

Card 2/3

APPROVED FOR RELEASE: 03/20/2001

CIA-RDP86-00513R000619130003-8"

Connection Between the Increase of an Entire Function of - 39-3-5/8

Many Variables and the Distribution of the Singularities of Its Associated Function

 \bar{s} $(-\varphi_1, \ldots, -\varphi_n) = \bar{s} (\varphi_1, \ldots, \varphi_n)$.

3 Soviet and 4 foreign references are quoted.

SUBMITTED: 11 June 1956

AVAILABLE: Library of Congress

1. Functions-Theory

Card 3/3

AFFROVED	FOR RELEASE: 03/20/2001 CIA-RDP00-00513R000019130003	-0
•	sov, 140 -58-3-13/34	
AUTHOR:	Ivanov, V.K. Uniqueness Theorem of the Inversion Problem of the Logarith-	5
TITLE:	mic Potential for Star Shaped by Sta	
	mnozhestv) Izvestiya vysshikh uchebnykh zavedeniy . Matematika, 1958,	
PERIODICAL:		1,000
	n is redial relative to the origin, then	
ABSTRACT:	ray arg $z = \theta$ contains a limit point $z = re^{i\theta}$ with $r < r_0$	
	lie in D. The function $r_0 = f(\theta)$ is called the defining	
	function of he had bounded, measurable sets which	
	are radial relative to the origin. If η are the defining external potential for the density $\gamma = 1$, then the defining functions $f_1(\theta)$ and $f_2(\theta)$ are identical for almost all values functions $f_1(\theta)$ and $f_2(\theta)$ are identical for almost all values	
	of 0. The proof is carried out according to the scheme of Novikov	
Card 1/2		
अस्ति। महन्तर्राहरूने स्वारंत्राहरूमा सन्देशना स्वारंहन		

Iniqueness Theorem of the Inversion Problem of the SOV/140-58-3-13/34

Iniqueness Theorem of the Inversion Problem of the SOV/140-58-3-13/34

Incomplete the Inversion Problem of the SOV/140-58-3-13/34

[Ref 1].

There are 7 Soviet references.

ASSOCIATION: Ural'skiy gosudarstvennyy universitet imeni A.M.Gor'kogo (Ural State University imeni A.M. Gor'kiy)

SUBMITTED: December 16, 1957

Card 2/2

507/140-58-4-11/30 Ivanov, V.K. AUTHOR: On the Stability of the Reversion Problem of the Logarithmic TITLE: Potential (Ob ustoychivosti obratnoy zadachi logarifmicheskogo potentsiala) PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Matematika, 1958, Nr 4, pp 96-99 (USSR) The sufficient conditions for the stability of the reversion ABSTRACT: problem of the logarithmic potential as well as the general problem are due to Tikhonov [Ref 3]. A completion to [Ref 3] is the paper of the author [Ref 4]. In the present paper the author gives examples of stability which can be reduced from the results of Tikhonov [Ref 3] and Ivanov [Ref 4]. There are 5 Soviet references. ASSOCIATION: Ural'skiy gosudarstvennyy universitet imeni A.M. Gor'kogo (Ural State University imeni A.M. Gor'kiy) December 16, 1957 SUBMITTED: Card 1/1

SOV/39-47-1-1/8 16(1) Ivanov, V.K. (Speciality) AUTHOR: The Characteristic of Increase of an Entire Function of Two Variables and its Application for the Summation of Double TITLE: Power Series (Kharakteristika rosta tseloy funktsii dvukh peremennykh i yeye prilozheniye k summimovaniyu dvoynykh stepennykh ryadov) PERIODICAL: Matematicheskiy sbornik, 1959, Vol 47, Nr 1, pp 3-16 (USSR) ABSTRACT: $F(z_1, z_2) = \sum_{m_0 n} \frac{a_{mn}}{m! n!} z_1^m z_2^n$ (1) $|F(z_1, z_2)| \leq Ae^{G_1|z_1|+G_2|z_2|}$, (2) where A, 61,62 are positive constants, $f(z_1, z_2) = \sum_{m,n} \frac{a_{mn}}{z_1^{m+1} z_2^{n+1}}$ (3)Let the plane $\Pi\left(\boldsymbol{\mathcal{P}}_{1},\boldsymbol{\mathcal{\mathcal{P}}}_{2}\right)$ consist of all points Card 1/4

SOV/39-47-1-1/8 The Characteristic of Increase of an Entire Function of Two Variables and its Application for the Summation of Double Power Series

 $z_1 = r_1^{i p_1}, \quad z_2 = r_2^{i p_2}$ for fixed φ , φ_2 and variable r_1 and r_2 . Let $T(\varphi_1, \varphi_2)$ be the set of those points $V=(V_1, V_2)$ of the plane $\Pi\left(\left.\phi_{1},\,\phi_{2}\right)\right.$, for which the following condition is satisfied: To every $v\in T(|\phi_1,|\phi_2|)$ there exists a positive constant A = A(v), so that for fixed φ_1, φ_2 and arbitrary r_1, r_2 there holds $|F(r_1e^{i\varphi_1}, r_2e^{i\varphi_2})| \leqslant Ae^{y_1r_1+y_2r_2}$ Let $C(\varphi_1, \varphi_2)$ be theset of those points c " (c_1, c_2) of $\Pi \ (\ \gamma_1,\ \gamma_2)$, which satisfy the following condition : All points $z=(z_1,z_2)$ of the four-dimensional space R_4 of the variables z_1,z_2 for which $Re(z_1e^{-i\frac{p_1}{p_1}}) \ge c_1$, $\operatorname{Re}(z_2^{-i}\varphi_2) \geqslant c_2^2$, are points of regularity of $f(z_1, z_2)$.

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CIA-RDP86-00513R000619130003-8" APPROVED FOR RELEASE: 03/20/2001

SOV/39-47-1-1/8

The Characteristic of Increase of an Entire Function of Two Variables and its Application for the Summation of Double Power Series

If the planes Π (ϕ_1 , ϕ_2) for different fixed ϕ_1 , ϕ_2 are brought to a coincidence by considering r_1 and r_2 in (4) as point coordinates in the coinciding plane, then the domains $T(\phi_1,\phi_2)$ and $C(\phi_1,\phi_2)$ can be compared for different systems of angles. Principal result: For a coincidence of $\Pi(\phi_1,\phi_2)$ and $\Pi(-\phi_1,-\phi_2)$ for the closures it holds:

 $\overline{T}(\varphi_1, \varphi_2) = \overline{C}(-\varphi_1, -\varphi_2).$

This result is a generalization of the well-known theorem of Polya / Ref 4 and, for n = 2, it improves a similar older result of the author / Ref 3 (less assumptions). In the last paragraph of the present paper the obtained results are used in order to determine the region of summation of a double power series with the aid of the

Card 3/4

SOV/39-47-1-1/8
The Characteristic of Increase of an Entire Function of Two Variables and its Application for the Summation of Double Power Series

integral method of Borel / Ref 1 / The construction method forms a ratural analogy of the polygon of Borel but the domain of summability is no longer convex.

There are 5 ref., 2 of which are Source, American, 1 German, and 1 French.

SUBMITTED: April 30, 1957

Card 4/4

analytic function of the variables \mathbf{z}_1 , \mathbf{z}_2 .

(1.1) $u(x_1, y_1, x_2, y_2) = Re f(z_1, z_2)$

Card 1/4

88182 S/140/60/000/006/008/018 C111/C222 16.3200 AUTHOR: Ivanov. V.K. On a Boundary Value Problem Connected With Analytic Functions of TITLES Two Complex Variables PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Matematika, 1960, No. 6, pp. 103 - 113 TEXT: Let $z_1 = x_1 + iy_1, z_2 = x_2 + iy_2$ (2.1)and $z_1 = r \cos \theta e$, $z_2 = r \sin \theta e$ Let K be the wedge $0 \le \arg z_j \le \alpha_j$, j = 1,2, in the z p-plane. Let the biwedge K be the topological product $K = K_1 \times K_2$. Let $f(z_1, z_2)$ be an

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On a Boundary Value Problem Connected With Analytic Functions of Two Complex Variables

is called a biharmonic function.

(1.3)
$$v(x_1, y_1, x_2, y_2) = \text{Re } f(\overline{z_1}, z_2)$$

is called an antibiharmonic function. Problem & Determine in K a function

(3.1)
$$W = r^{\S} H(\theta, \Psi_1, \Psi_2) = r^{\S} H^{(1)}(\theta, \Psi_1, \Psi_2) + r^{\S} H^{(2)}(\theta, \Psi_1, \Psi_2)$$

which satisfies the following conditions : 1)

(3.2)
$$u = r^{g} H^{(1)}(\theta, \varphi_1, \varphi_2)$$
 and $v = r^{g} H^{(2)}(\theta, \varphi_1, \varphi_2)$

are biharmonic and antiharmonic, respectively: 2) (3.3)
$$H^{(1)}(0, \varphi_1, \varphi_2) = O(0^{-\epsilon})$$
, $H^{(2)}(0, \varphi_1, \varphi_2) = O(0^{-\epsilon})$

for
$$0 \rightarrow 0$$
, $H^{(1)}(0, \varphi_1, \varphi_2) = O\left(\left(\frac{\widetilde{k}}{2} - \theta\right)^{-\epsilon}\right)$, $H^{(2)}(0, \varphi_1, \varphi_2) = O\left(\left(\frac{\widetilde{k}}{2} - \theta\right)^{-\epsilon}\right)$

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的结果是要转进器管理的设计的原则是是经验的支持性的现在,可以通过的企业,可以通过的企业,但是不是不是一个企业的企业,但是不是一个企业的企业,但是不是一个企业的企业,

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On a Boundary Value Problem Connected With Analytic Functions of Two Complex Variables

for $0\to \frac{1}{2}$, where £ is an arbitrary positive number. 3) For an approximation to the topological product of the boundaries of K_1 and K_2 , for almost all 0, wassumes prescribed boundary values

$$(3.4) \begin{array}{c} w(r,0,0,0) = r^{\frac{9}{5}} h_{00}(\theta) , & w(r,0,0,\infty_{2}) = r^{\frac{9}{5}} h_{01}(\theta) \\ w(r,0,\infty_{1},0) = r^{\frac{9}{5}} h_{10}(\theta) , & w(r,0,\infty_{1},\infty_{2}) = r^{\frac{9}{5}} h_{11}(\theta) \end{array}$$

where $h_{\lambda \mu}$ (9) are measurable functions uniformly bounded for almost all 9.

(4)
$$0 < g < \frac{\tilde{\mu}}{d_j}$$
, $j = 1, 2,$, where d_j is the opening angle of K_j .

After introducing a new variable $t=\ln tg \theta$ the author proves the existence of the solution by applying complex Fourier transformations in t. The proof of uniqueness is given with the aid of the principle of Phragmen-Lindelöf which is extended to the functions Card 3/4

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s/140/60/000/006/008/018 C111/C222

On a Boundary Value Problem Connected With Analytic Functions of Two Complex Variables

$$f(z_1,\overline{z_1},z_2) = f_1(z_1,z_2) \cdot f_2(\overline{z_1},z_2) , |f(z_1,\overline{z_1},z_2)| \leq M_1$$

The continuous dependence of the solution on the inital conditions is proved.

The author mentions B.Ya.Levin. There are 3 references: 2 Soviet and 1 English.

ASSOCIATION: Ural'skiy gosudarstvennyy universitet imeni A.M. Gor'kogo (Ural State University imeni A.M. Gor'kiy)

SUBMITTED: December 20, 1958

Card 4/4

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On the growth indicatrix ...

where $F_1(z_1,z_2)$ and $F_2(\overline{z}_1,z_2)$ are entire functions of their arguments. Let M(r) be the maximum of the absolute value of $F(z_1, \overline{z}_1, z_2)$ on $|z_1|^2 + |z_2|^2 = r^2$. The order and type of $F(z_1, \overline{z}_1, z_2)$ are defined by

$$S = \frac{\lim_{r \to \infty} \frac{\ln \ln M(r)}{\ln r}}{\ln r}$$
 (2.4)

$$6 = \frac{1 \text{ im}}{1 \text{ im}} \frac{\ln \mathbf{u}(\mathbf{r})}{\mathbf{r}^g} . \tag{2.5}$$

It is assumed that

$$9 < \frac{\pi}{\alpha_1}$$
, $9 < \frac{\pi}{\alpha_2}$, $6 < +\infty$ (2.6)

is always satisfied.

h(0,
$$\varphi_1$$
, φ_2) = $\frac{1}{1}$ $\frac{\ln |F(r \cos \theta e)|}{r \rightarrow \infty}$, $\frac{i\varphi_1}{r}$, $\frac{-i\varphi_1}{r}$, $\frac{i\varphi_2}{r}$

is called the growth indicatrix of F(z1, 21, 22). Card 2/4

On the growth indicatrix...

s/140/61/000/002/001/009 C111/C222

Theorem 1: For every fixed system of the values φ_1 and φ_2 the growth indicatrix $h(\theta, \varphi_1, \varphi_2)$ of $F(z_1, \overline{z_1}, z_2)$ is summable with respect to θ in the interval [0, T].

Let Q be the region which is cut out of the unit sphere r=1 by the biwedge K. The totality of the four lines

$$0 \le 0 \le \frac{\pi}{2}$$
, $\varphi_1 = 0 \text{ or } \alpha_1$, $\varphi_2 = 0 \text{ or } \alpha_2$ (4.2)

is called the skeleton L of Q. Theorem 2: Let $h(0, \, \phi_1, \, \phi_2)$ be the growth indicatrix of the function $F(z_1,z_1,z_2)$ of finite order ξ and type δ , let Q be the region defined by

$$0 \leqslant 0 \leqslant \frac{\pi}{2}, \quad 0 \leqslant \varphi_1 \leqslant \alpha_1, \quad 0 \leqslant \varphi_2 \leqslant \alpha_2, \quad (4.1)$$

where

where $\alpha_1<\frac{\pi}{9}\;,\quad \alpha_2<\frac{\pi}{3}.$ Then there exists a single bispherical function H(0, φ_1 , φ_2) with the properties

1) on L it holds
$$H(0;L) = h^{*}(0;L); \qquad (6.1)$$

Card 3/4

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On the growth indicatrix...

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C111/C222

2) in Q-L it holds

h(θ, φ₁, φ₂) ≤ H(θ, φ₁, φ₂)...

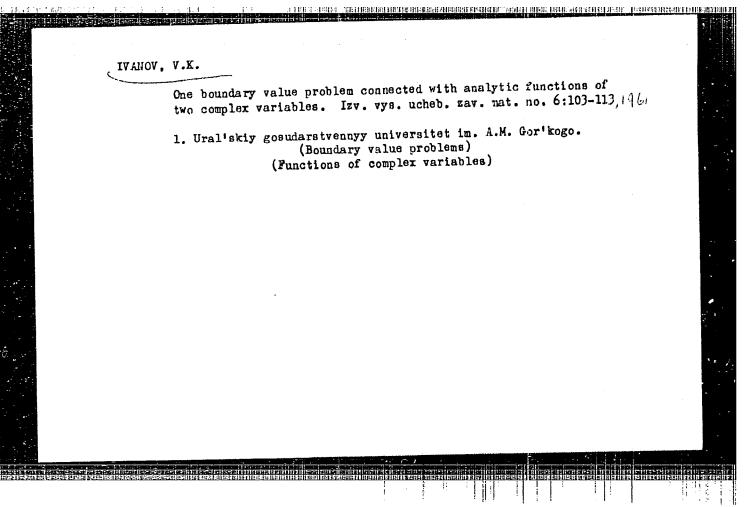
Theorem 2 shows that the growth indicatrix defined by (2.7) indeed has a property analogous to the trigonometric convexity.

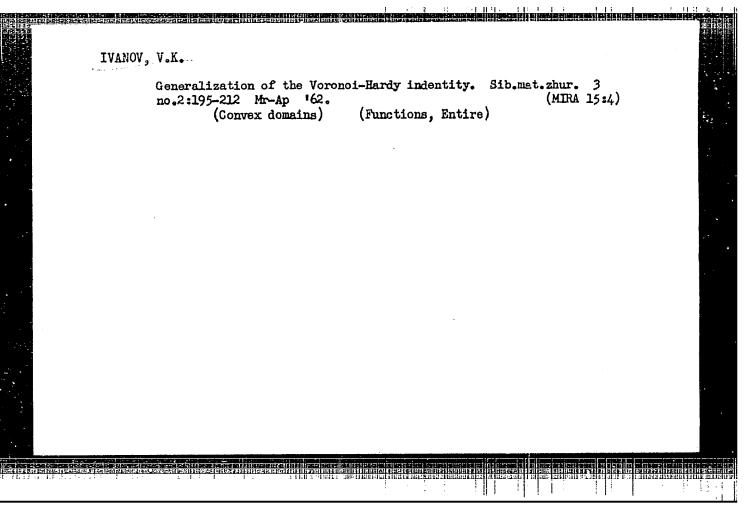
The author mentions A.A.Temlyakov. There are 3 Soviet-bloo references.

ASSOCIATION:Ural'skiy gosudarstvennyy universitet im.A.M.Gor'kogo (Ural State University im.A.M.Gor'kiy)

SUBMITTED: January 27, 1959

Card 4/4





34824

S/020/62/142/005/003/022 B112/B102

16.4600

AUTHOR: IV

Ivanov. V. K.

TITLE:

Integral equations of the first kind and approximate

solution of the inverse potential problem

PERIODICAL: Akademiya nauk SSSR. Doklady, v. 142, no. 5, 1962, 998-1000

TEXT: The equation $Ax_0 = y_0$ with a discontinuous inverse operator A^{-1} is investigated. It is assumed that a sequence $M_1^c M_2^c \dots c M_n^c$... of closed sets M_n exists such that x_0 is a limit point of the sum

 $\sum_{n=1}^{\infty} M_n$ Minimum values x_n of $||Ax - y_0||$ on M_n can be regarded as

approximate solutions of Ax_o = y_o. As an example, the inverse plane potential problem is considered. Reference is made to I. M. Lavrent'yev

(DAN, 127, No. 1, 31 (1959)) and P. S. Novikov(DAN, 18, No. 3, 165 (1938)). There are 6 references: 3 Soviet and 3 non-Soviet. The three references

Card 1/2

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Integral equations of the first kind and ... B112/B102

to English-language publications read as follows: J. Douglas, T. M. Gallie, Duke Math. J., 26, No. 3, 339 (1959); M. Frank, Ph. Wolf, Naval Res. Logistics Quarterly, 3, 95 (1956); J. B. Rosen, Bull. Am. Math., Soc., 63, No. 1, 15 (1957).

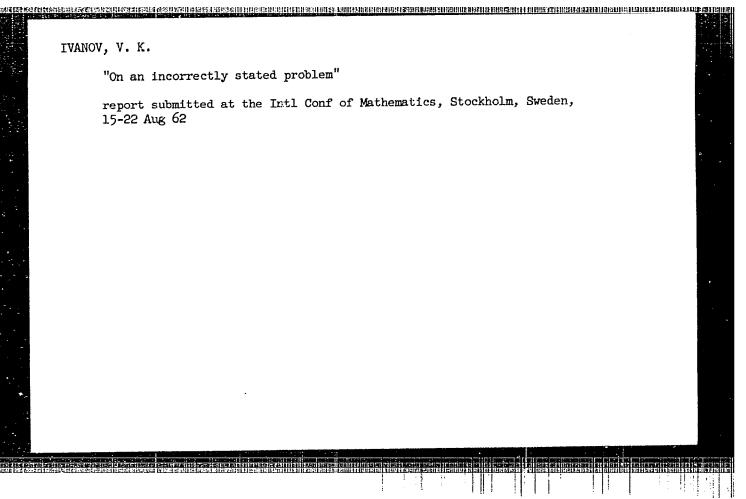
ASSOCIATION: Ural'skiy gosudarstvennyy universitet im. A. M. Gor'kogo

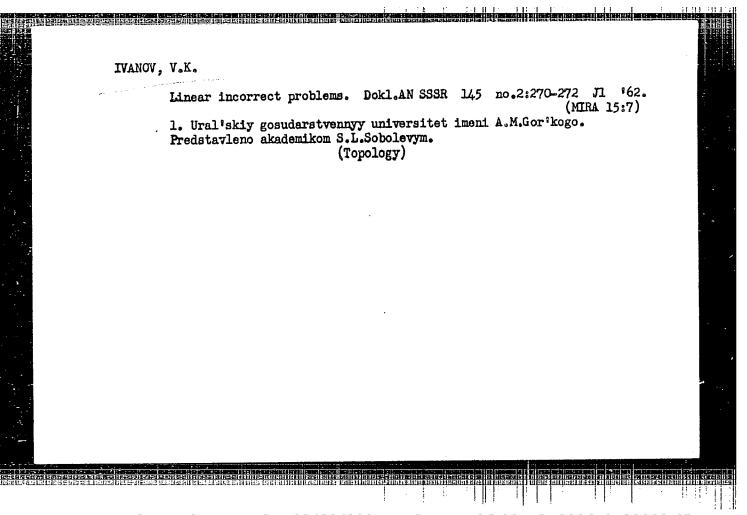
(Ural State University imeni A. M. Gor'kiy)

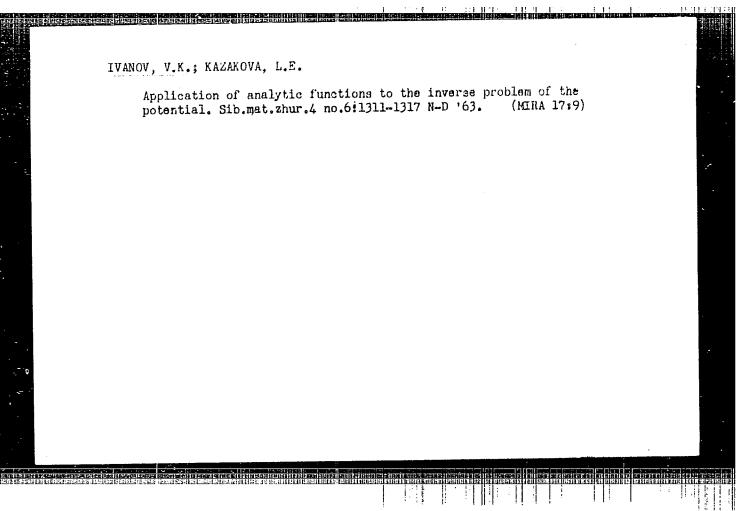
PRESENTED: October 23, 1961, by S. L. Sobolev, Academician

SUBMITTED: October 14, 1961

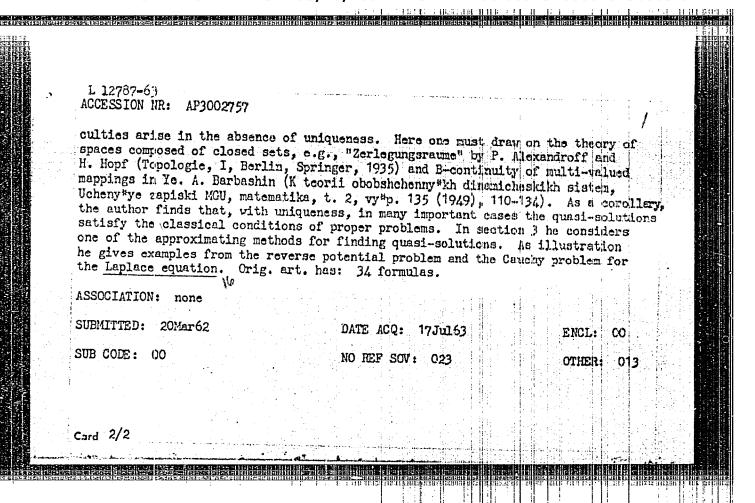
Card 2/2

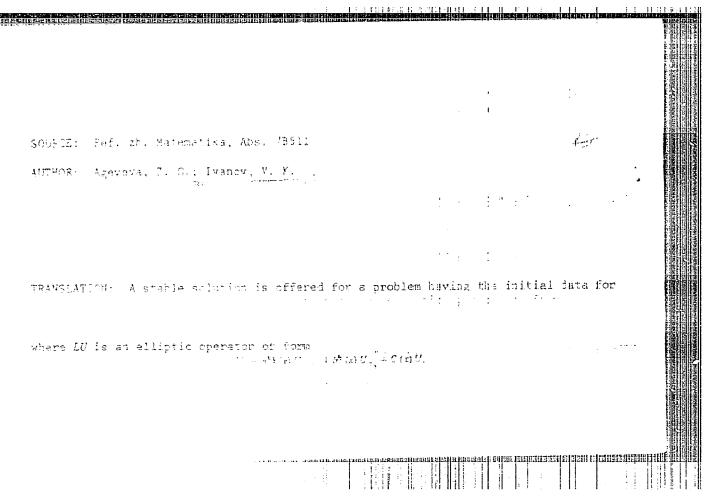


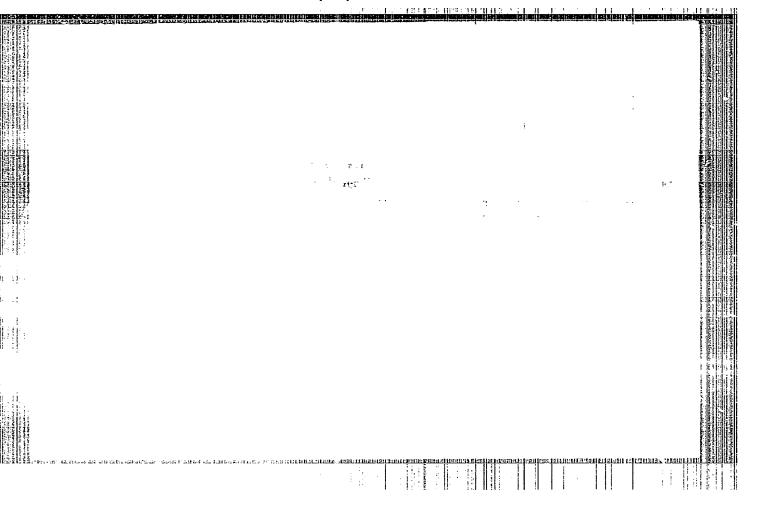




ы**р(с)** ... EAT(d)/FCC(w)/BDS AFFTC 8/0039/63/061/002/0211/0223 AP3002757 Myanov, V. K. (Sverdlovsk) AUTHOR: Improperly stated problems 16 TITLE: SOURCE: Matematicheskiy sbornik, v. 61, no. 2, 1963, 211-223 TOPIC TAGS: partial differential equation, improperly stated problem, potential problem, Beta-stability, best approximation, quasi-solution ABSTRACT: A properly stated problem in partial differential equations of mathematical physics is one whose solution satisfies the following conditions: .1) it exists, 2) it is unique, and 3) it depends continuously on the initial data (it is stable). In modern applications many problems arise which cannot be properly stated. The majority of improperly stated problems can be reduced to integral or functional equations of first order. Section 1 deals with proper statements. Various improper problems are discussed, and a new statement is given which consists of substituting a best approximation for the exact solution. The quasi-solution given in this section is a generalization of the usual solution and coincides with the true solution when the latter exists. In section 2 the author shows that the quasi-solution has stability in the usual sense (Beta-stability). The main diffi-Card 1/2







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L 571195-65 ENT(d)/T IJP(c)

ADDRESS TOW TRY APPOLIZOUS

UR/0376/65/001/001/01/31/01/56

AUTHOR: DIRECT, V. K.

TITEM: Cauchy problem for the Laplace equation in an infinite wards

SOURCE: D.fferentaial nyre unavaniya, v. 1, no. 1, 1965, 131-136

TOPIC TAGS: differential equation, Laplace equation

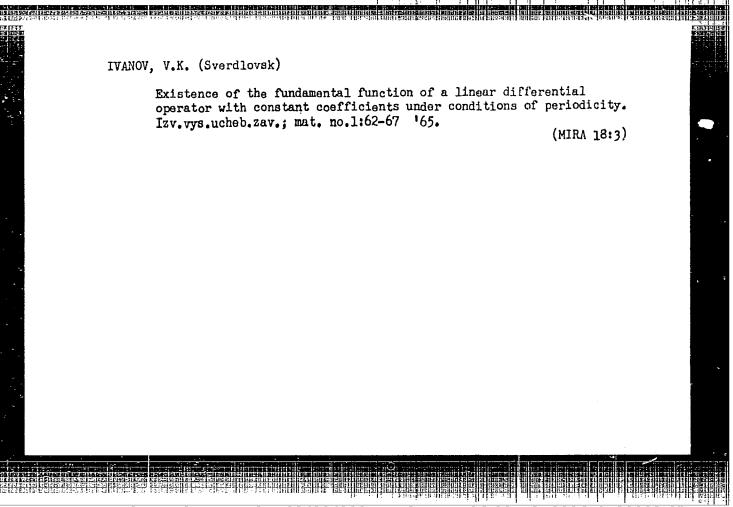
ARSTHACT: Using a generalised function type regularization, the eather is able to precede from a classical solution of

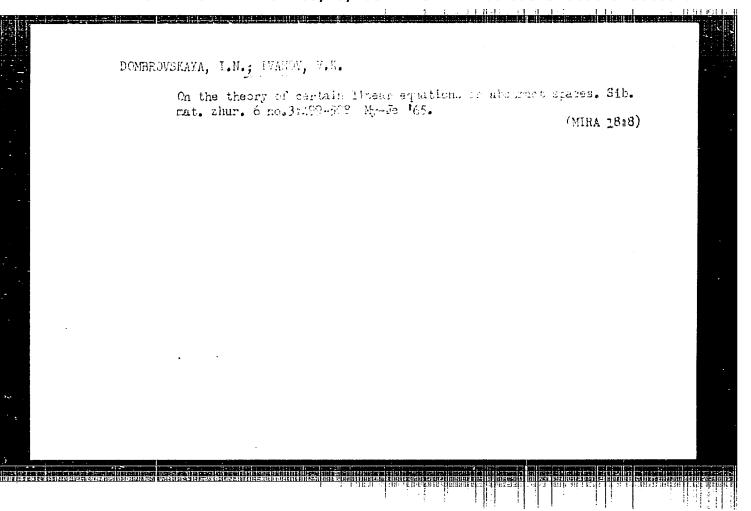
$$\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} = 0$$

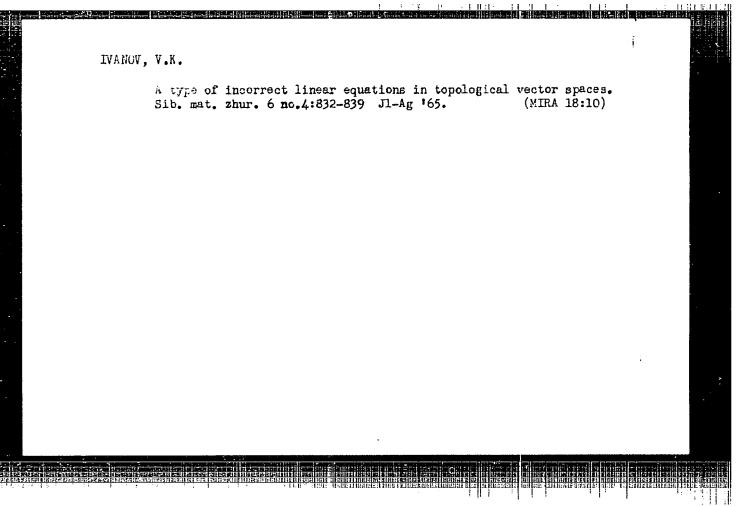
subject to $u(x_i0)$ of f(x), $u_i^*(x_i0)$ of g(x) where f and g are analytic in - m (if the first of this exciption which fourther the first of the

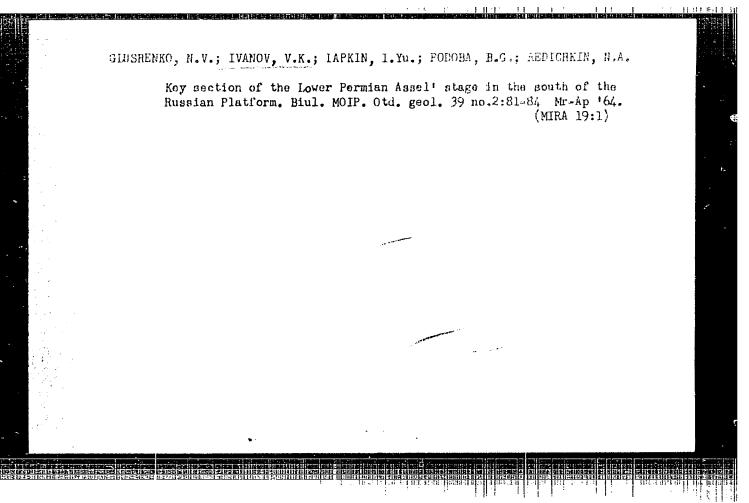
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L 07257-67 EWT(d) IJP(e)SOURCE CODE: UR/0208/66/006/003/0570/0576 ACC NR: AP6018636 AUTHOR: Dolgopolova, T. F. (Sverdlovsk); Ivanov, V. K. (Sverdlovsk) ORG: none 1<u>/</u> TITLE: Numerical differentiation SOURCE: Zhurnal vychislitel'noy matematiki i matematicheskoy fiziki, v. 6, no. 3, 1966, 570-576 TOPIC TAGS: numeric solution, differentiation error, approximation calculation, approximation error ABSTRACT: Various articles dealing with numerical differentiation substitute the function f(x), which is to be differentiated, by an approximation polynomial p(x), and this is followed by an estimate of the |f'(x) - p'(x)| error. However, unlike integration, numerical differentiation belongs to inaccurate problems: one can always find cases where for an arbitrarily small deviation of the known approximate function $f_{\delta}(x)$ from the exact one f(x) their derivatives may differ by an arbitrarily large amount. Consequently, there is a need for a theory of inaccurate problems. The present authors use a modification of the regularizing method due to A. N. Tikhonov (Dokl. AN SSSR, 1963, 151, no. 3, 501-504) which permits the establishment of a polynomial $p_{\delta}(x)$, uniformly approaching f'(x), from the function $f_{\delta}(x)$. In this modification, an operator equation of the first kind is solved in which instead of requiring UDC: 518:517.949.12 Card 1/2

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ACC NR: AT6023742 (A,N) SOURCE CODE: UR/2755/66/000/005/0163/0172	
AUTHOR: Beskorovaynyy, N. M.; Ivanov, V. K.; Petrashko, V. V.	
ORG: none	
R+I	
TITLE: Corrosion of chromium-nickel stainless steel in lithium	
SOURCE: Moscow. Inzhenermo-fizicheskiy institut. Metallurgiya i metallovedeniye chistykh metallov, no. 5, 1966, 163-172	·
TOPIC TAGS: stainless steel, chromium-nickel-steel, steel corrosion, lithium induced corrosion, comusion resistance, and, chromium steel, nickel, steel, lithium, corrosion, comusion	
ABSTRACT: Three series of 1Kh18N9T stainless-steel specimens were tested for corrosion behavior in lithium at 700C for 10 or 200 hr. Series 1 and 2 specimens were tested in lithium containing a small amount of C ¹⁴ isotope and in tanks made of	
1Kh18N9T steel (series 1) or Armco-iron (series 2). In the case of series 3 specimens, the lithium contained 0.1% carbon in addition to C ¹⁴ and the tanks were made	
of Armco-iron. The corrosion was found to follow the same pattern under all the conditions tested, and was characterized by a gradual dissolution of chromium and	
nickel from the surface layer of the specimens. With decreasing chromium and nickel content the steel changes its structure and gradually loses its corrosion	
resistance. Microporosity formed in points previously occupied by chromium and nicke	1
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Card 1/2	

lowers considerably the steel ductility. The carbon content in lithium and tank material were found to have a marked effect on the intensity of processes associated with corrosion. The most intensive loss of chromium and nickel was observed in series 2 and 3 specimens in which in 200 hr the chromium content in the surface layer dropped by 50% and the nickel content, by 45 and 50% of the original content, respectively. Specimens of series 1 under the same conditions lost 10% of their chromium and 30% of their nickel 2 Accordingly, the elongation of the series 1, 2, and 3 2 specimens dropped from the original 48.2% to 47.1, 26.4, and 24.4%, respectively. Carbon contained in lithium was found to diffuse into the steel. However, in the first hours of the test, carbon concentrates primarily in the surface layer. As the chromium content in the surface layer drops, carbon migrates inside, following the front of original chromium content. Orig. art. has: 7 figures and 4 tables. [DV] SUB CODE: 11/ SUBM DATE: none/ ORIG REF: 005/ ATD PRESS: 584/	L 37699-66 ACC NR: AT6023742	
dropped by 50% and the nickel content, by 45 and 50% of the original content, respectively. Specimens of series 1 under the same conditions lost 10% of their chromium and 30% of their nickel 2 Accordingly, the elongation of the series 1, 2, and 3 27 specimens dropped from the original 48.2% to 47.1, 26.4, and 24.4%, respectively. Carbon contained in lithium was found to diffuse into the steel. However, in the first hours of the test, carbon concentrates primarily in the surface layer. As the chromium content in the surface layer drops, carbon migrates inside, following the front of original chromium content. Orig. art. has: 7 figures and 4 tables. [DV] SUB CODE: 11/ SUBM DATE: none/ ORIG REF: 005/ ATD PRESS:554/	lowers considerably the steel ductility. The carbon content in lithium and tank material were found to have a marked effect on the intensity of processes associated with corrosion. The most intensive loss of chromium and nickel was observed in	
first hours of the test, carbon concentrates primarily in the surface layer. As the chromium content in the surface layer drops, carbon migrates inside, following the front of original chromium content. Orig. art. has: 7 figures and 4 tables. [DV] SUB CODE: 11/ SUBM DATE: none/ ORIG REF: 005/ ATD PRESS:5554/	dropped by 50% and the nickel content, by 45 and 50% of the original content, respectively. Specimens of series 1 under the same conditions lost 10% of their chromium and 30% of their nickel 2 Accordingly, the elongation of the series 1, 2, and 3 27 specimens dropped from the original 48.2% to 47.1, 26.4, and 24.4%, respectively.	
	first hours of the test, carbon concentrates primarily in the surface layer. As the chromium content in the surface layer drops, carbon migrates inside, following the front of original chromium content. Orig. art. has: 7 figures and 4 tables. [DV]	2
1	SUB CODE: 11/ SUBM DATE: none/ ORIG REF: 005/ ATD PRESS:554/	

Card 2/2

BUTKIN, Ye.I., kand.veterinarnykh nauk; Prinimal uchastiye IVANOV, V.L., vrach-bakteriolog

Effectiveness of living antipasteurellosis vaccine. Veterinariia 39 no.12:37-38 D '62. (MIRA 16:6)

1. Kurskaya oblastnaya nauchno-proizvodstvennaya veterinarnaya laboratoriya.

(Kursk Province--Chicken chglera--Preventive inoculation)

ACCESSION NR: AP3000496

\$/0145/63/000/001/0117/0129

AUTHOR: Ivanov, V. L. (Candidate of technical sciences)

TITLE: Investigation of heat transfer in a closed channel with natural convection and changing composition of the heat conducting medium

SOURCE: Izv. VUZ: Mashinostroyemiye, no. 1, 1963, 117-129

TOPIC TAGS: heat transfer, closed channel heat transfer, film condensation, natural convection, evaporation heat transfer, turbine blade cooling

ABSTRACT: Experimental and theoretical investigations were performed on heat transfer in closed channels with natural convection during change of state of the conducting medium. Of particular interest was the application of this process to cooling of gas turbine blades. The convection loop in a closed channel is set up as follows. The medium is evaporated at the hot end, and the vapors rise towards the cold end, are condensed, and flow down in a film along the walls. The fluid was air heated and either air cooled or water cooled. Water and HCO₂CH₃ were used as the heat transfer medium. The following observations were made: F) a film did form along the length of a channel and vapor rose in the center; 2) depending on the

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ACCESSION NR: AP3000496

Card 2/3

amount of fluid in the apparatus, the fluid film would cover all the heated section (2-2.5 cm³ water) and cool, or it would just reach the heated section (less than 2 cm³) and provide no cooling, or it would form a column on the bottom which periodically surged up (more than 2.5 cm³) but would provide the same cooling; 3) the temperature in the apparatus settles on the temperature of the saturated liquid at the chamber pressure; 4) for less than 3 cm³ of water the film could be broken by wall imperfections (thus disrupting the cooling process). For 3 cm³ and more the surging column would restore the film. Based on these observations, a theoretical model was established, and the equations were derived. The average heat transfer coefficients along the length were found from Nu_e = 0.67 x C_i (Ar · Pr · K)^{0.25}, where Nu_e = Nusselt number, Ar = Archimedes number, Pr = Prandtl number, K = Kirpichev number, and C_i was derived for cylindrical and flat channels (it varied from 1.4 - 0.4 for different conditions). The effects of Coriolis force and of centrifugal force in a rotating model were considered, and both the static and rotating models were studied experimentally. As predicted, it was found that in a rotating model the fluid film could not be disturbed by imperfections and that

ACCESSION NR: AP3000496

Coriolis forces produced no ill effects. Orig. art. has: 9 figures and 7 formulas.

ASSOCIATION: MVTU im. N. E. Baumane (MVTU)

SUBMITTED: 25Apr62

DATE ACQ: 21Jun63

EXCT: 00

SUB CODE: PH

NO REF SOV: OOL

THER: 002

Cord 3/3

KAPLAH, V.V.; NASHATYR', V.M.; IVAHOV, V.L.

Methods of synthetic testing of high-voltage switches for their disconnecting ability. Izv. vys. ucheb. zav.; elektromekh. 1 no.5:63-71 '58. (MIRA 11:8)

(Electric switchgoar--Testing)

1110-58-6-7/22 Kaplan, V.V., Nashatyr', V.M., Candidates of Technical Sciences and Ivanov, V.L., Engineer. AUTHORS: Switching Over-voltages When Using Small-oil-volume TITLE: Circuit-breaker Type MG-110 to Disconnect Unloaded Transformers and Lines (Kommutatsionnyye perenapryazheniya pri otklyuchenii malomaslyanym vyklyuchatelem tipa MG-110 nenagruzhennykh transformatorov i liniy) Vestnik Elektropromyshlennosti, 1958, PERIODICAL: pp 31 - 37 (USSR) Over-voltages that are set up when switching unloaded ABSTRACT: lines and transformers largely determine the insulation level. Over-voltage measurements can rarely be made on full-scale systems and laboratory tests of circuit-breakers are therefore necessary. The article describes tests on a 110-kv small-oilvolume circuit breaker of 2 500 MVA, type MG-110, built by the Elektroapparat Works, breaking small inductive and capacitive currents. The tests were made in the Gorev laboratory of the Leningradskiy politekhnicheskiy institut (Leningrad Polytechnical Institute) on equivalent circuits specially designed for this application and using oscillatory circuits as the source of e.m.f. Card 1/7

110-58-6-7/22 Switching Over-voltages When Using Small-oil-volume Circuit-breaker Type MG-110 to Disconnect Unloaded Transformers and Lines

The circuit of Figure 1 was employed in experiments on disconnecting an unloaded transformer. As the oscillatory circuit can provide undamped oscillations for only a short time, the test must be so arranged that steady no-load current flows in the transformer as soon as possible after it is connected to the supply. Therefore, the transformer is connected through a damping resistance. The first tests were made with the transformer de-magnetised by a special procedure. The test procedure is fully described. The circuit-breaker was tested under singlephase conditions, to represent disconnection by one pole of the circuit-breaker of a transformer with grounded neutral. The test voltage equalled the system phase-voltage. To represent tests on transformers with unearthed neutral, some of the tests used a voltage of one-and-a-half times the system voltage. Tests were made with one arc-quenching chamber and with two connected in series. Other tests corresponded to disconnection of three-phase transformers with earthed and isolated neutral, with outputs of 31.5 to 189 MVA. The current amplitude ranged from 6 to 64 A.

Cars 2/7

Switching Over-voltages When Using Small-oil-volume Circuit-breaker Type MG-110 to Disconnect Unloaded Transformers and Lines

The circuit-breaker was tested both with and without arrangements for high-speed reclosure. The results of all the tests are summarised in Figure 2. They show that both types of small-oil-volume circuit-breaker successfully break transformer magnetising current without appreciable over-voltages. In most tests, the over-voltage was not more than double the normal power-frequency voltage and in one case, only, it rose to 240%. For a given value of current there is considerable scatter of the time for which the arc burns: in most cases it was from 0.01 to 0.03 sec and only occasionally did it rise to 0.04 sec when the current was more than 30A. The relationship between the over-voltage factor on the transformer and the number of occurrences as a percentage of the total is plotted in Fig. 3, which shows that, over the current range 5 - 15 A, the highest over-voltage was 134% of the normal value. Oscillograms showed that the current was interrupted somewhat before the current would normally pass through zero and whilst it still had some finite value. This effect is important in evaluating the operation of switchgear, since Card3/7

110-58-6-7/22 Switching Over-voltages When Using Small-cil-volume Circuit-breaker Type MG-110 to Disconnect Unloaded Transformers and Lines

the instantaneous-current value at the instant of interruption largely governs the transformer over-voltage. Many
attempts have been made to explain the phenomena of
interrupting small inductive currents, but none is completely
convincing. Typical current oscillograms at the instant of
interruption are shown in Figure 4 and indicate that the
effect of interruption at a finite current value may occur
whether or not high-frequency oscillations are present.
The conditions under which the arc becomes unstable in this
way are discussed.
The process of this kind of interruption can be characterised by a system of differential equations relating the

The process of this kind of Interruption can be that determined by a system of differential equations relating the circuit-breaker current and the transformer inductive and capacitative currents. Calculated curves of the current at the moment of interruption are plotted in Figure 5 for the initial conditions of the oscillograms of Figures 4a and 4b. A comparison of curves 5a and 4a shows that the calculated current curves are near enough to the experimental ones. The time interval from the instant of start of fall

Card4/7

110-5%-6-7/22 Switching Over-voltages When Using Small-oil-volume Circuit-breaker Type MG-110 to Disconnect Unloaded Transformers and Lines

of current to zero current is the same in both cases. Thus, it follows that the presence of high-frequency oscillations does not determine whether the current is interrupted before the normal zero, as is required by current theories of the subject. The new explanation offered in the article does not preclude occurrence of preliminary high-frequency oscillations but suggests that the mode of current interruption in any particular case depends on the conditions and that even with given conditions considerable scatter is observed.

Investigations on the circuit-breaker when disconnecting unloaded lines were made on an equivalent circuit with concentrated constants, as shown in Figure 6. The requirements that must be met to reproduce the actual conditions are stated and can be satisfied by this circuit. The source of undamped sinusoidal e.m.f. is a system of interconnected oscillatory circuits. Both types of breaker were tested whilst repreducing the conditions of an unloaded line of 200 km, which is about the longest Soviet 110-kV line. The power-frequency current interrupted was up to 40 A. The arc-suppression

Card5/7

110-58-6-7/22 Switching Over-voltages When Using Small-oil-volume Circuit-breaker Type MG-110 to Disconnect Unloaded Transformers and Lines

device of the small-oil-volume 220-kV circuit-breakers developed by the Elektroapparat Works (type MG-220) has four series arc-suppression chambers of the same construction as that used in the 110-kV breaker: hence, it was decided to verify the performance of the 220-kV breaker on a circuit equivalent to open lines 400 km long. The tests were made on a single arc-suppression chamber and preliminary tests showed that such partial testing is accurate enough for practical purposes. In no case, did the over-voltage exceed double the normal value and the arc is finally interrupted before the contacts reach the fully-open position. Power-frequency current is usually interrupted at the first current-zero; then the arc usually re-strikes and finally the high-frequency interruption takes place, without, however, giving rise to high over-voltages. This re-striking effect is of a highly statistical nature; it may or may not occur under given conditions and the duration of the current also varies. Similar observations have been made by the Swedish ASEA company when testing small-oilvolume circuit breakers. Card6/7

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Switching Over-voltages When Using Small-oil-volume Circuit-breaker Type MG-110 to Disconnect Unloaded Transformers and Lines

> On the basis of all the tests made, it is concluded that small-oil-volume circuit-breakers, types MG-110 and MG-110B successfully disconnect unloaded transformers and lines without giving rise to dangerous over-voltages. There are 6 figures and 6 references, 1 of which is Soviet, 2 German and 3 English.

ASSOCIATION: Leningradskiy politekhnicheskiy institut

(Leningrad Polytechnical Institute)

SUBMITTED:

July 29, 1957 1. Circuit breakers—Test results Card 7/7

8(2) AUTHORS:

Kaplan, V. V., Candidate of Technical SOV/105-58-11-7/29

Sciences, Nashatyr', V. M., Candidate of Technical Sciences,

Ivanov, V. L., Engineer

TITLE:

A Synthetic Method of Testing High-Voltage Switches

(Sinteticheskiy metod ispytaniya vysokovol tnykh vyklyuchateley)

PERIODICAL:

Elektrichestvo, 1958, Nr 11, pp 29-35 (USSR)

ABSTRACT:

In 1957 a wiring circuit was elaborated and put into practice at the Laboratoriya tekhniki vysokikh napryazheniy imeni Goreva Leningradskogo politekhnicheskogo instituta (Laboratory for

High-Voltage Engineering imeni Gorev at the Leningrad

Polytechnic Institute) on the basis of an oscillatory circuit.

This makes it possible to test quick-break switches by

synthetical means. The switches operate with a single automatic reclosure cycle (switching off - switching on - switching off). Conditions for carrying out equivalent synthetical switch tests in the automatic reclosure cycle and the basic wiring scheme of the testing device are described. The synthetic scheme was checked in connection with the testing of air-switches. The

checked in connection with the testing of air-switches. The oscillogram obtained shows that with lacking compensation of

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current- and voltage reduction the amplitude of the switching-off

A Synthetic Method of Testing High-Voltage Switches SOV/105-58-11-7/29

current at the third operation of the automatic reclosure cycle is smaller by about 25% than that of the initial current. The re-established voltage is reduced by the same amount with respect to the initial voltage. - When testing switches by means of compensating circuits, the reduction of current and voltage is entirely avoided. The amplitudes of all three currents as well as the initial and re-established voltages have the same values. The electron beam oscillograms show that the synchronizing devices worked out permit a very accurate adjustment of the testing device. There are 6 figures and 3 Soviet references.

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ASSOCIATION:

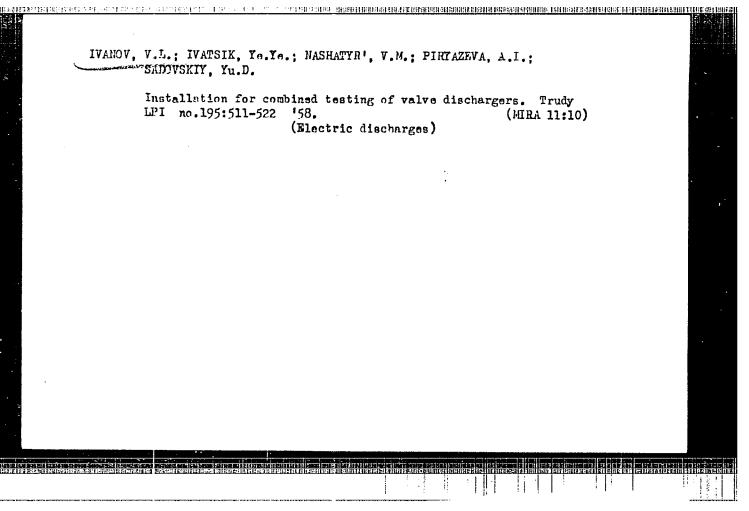
Leningradskiy politekhnicheskiy institut

(Leningrad Polytechnic Institute)

SUBMITTED:

January 20, 1958

Card 2/2



8(2) AUTHORS: Ivanov, V. L., Engineer, Nashatyr', V. M., SOV/105-59-7-16/30 Candidate of Technical Sciences, Polovoy, I. F., Candidate of

Technical Sciences

TITLE:

Some Problems of the Method of Testing High-voltage Insulation (Nekotoryye voprosy metodiki ispytaniy vysokovol'tnoy izolyatsii)

PERIODICAL:

Elektrichestvo, 1959, Nr 7, pp 61 - 64 (USSR)

ABSTRACT:

Three circuit diagrams of test devices are described, which were developed at the laboratory for high-voltage engineering imeni Gorev at the Leningradskiy politekhnicheskiy institut (Leningrad Polytechnic Institute). Also the results obtained by investigations of their mode of operation are given. Most internal overvoltages, which are characteristic of 110 - 500 kv mains, may be represented with an accuracy that is sufficient for practical use as the sum of voltages of various frequencies and amplitudes, among them also of direct voltages. It is therefore possible to reproduce them by means of circuits which are based on the addition of these components, i.e. on the connection in series of some e.m.f. sources with the object to be investigated. Figure 1 shows the most simple circuit of an apparatus for the investigation of insulation in the case of internal overvoltages. The device is

Card 1/3

Some Problems of the Method of Testing High-voltage Insulation SOV/105-59-7-16/30

described. Such a circuit is difficult to construct if high test voltages are required, because for this purpose a reactor with high inductivity for very high voltages and a rectifying device for a high voltage is necessary. The circuit shown in figure 2 satisfies these conditions. According to this circuit, a test device with 5 oscillatory circuits was built. Figure 5 shows the third wiring diagram, in the case of which capacity, inductivity, and charging device for considerably lower voltages are used than in the circuit shown by figure 2. Therefore, it is possible in this case to select optimum parameters of the oscillatory circuit. However, the test-transformer must be suited for a considerably higher voltage. According to the circuit shown by figure 5, a device with a test transformer was constructed. The corresponding oscillograms for the circuits shown by figures 2 and 5 are given. On the basis of the investigation it was found that the production of circuits for the testing of various types of high-voltage insulation with voltages corresponding to the shape, size, and duration of internal overvoltages in the electric mains, presents no technical difficulties, and requires a comparatively uncomplicated equipment (reactors, condensers, etc). There are 6 figures and 7 references, 4 of which are Soviet.

Card 2/3

Some Problems of the Method of Testing High-voltage Insulation SOV/105-59-7-16/30

ASSOCIATION:

Leningradskiy politekhnicheskiy institut im. Kalinina (Leningrad Polytechnic Institute imeni Kalinin)

SUBMITTED:

February 10, 1959

Card 3/3

IVANOV, V.L., inzh.

Effect of cooling on the hydraulic characteristics of a gas turbine.

1.2v.vys.ucheb.zav.; mashinostr. no.2:31-39 160. (MIRA 14:4)

1. Moskovskoye vyssheye tekhnicheskoye uchilishche imeni Baumana.

(Gas turbines--Cooling)

KAPIAN, V.V., kand.tekhn.nauk (Leningrad); NASHATYR', V.M., kand.tekhn.nauk (Leningrad); IVANOV, V.L., inzh. (Leningrad)

Statistical method for substantiating the selection of voltage in testing the interrupting capacity of circuit breakers.

Elektrichestvo no.2:69-73 F '60. (MIRA 13:5)

(Electric circuit breakers)

ALEKSANDROV, G.N., kand.tekhn.nauk; IVANOV, V.L., inzh.

Study of the electrical strength of air gaps and suspension insulators in the presence of internal overvoltages.

Elektrichestvo no.9:33-38 S '62. (MIRA 15:9)

1. Leningradskiy politekhnicheskiy institut imeni Kalinina.

(Electric lines-Overhead)
(Electric insulators and insulation)

L 11260-63 EMP(r)/EWT(1)/BDS--AFFTC/ASD

ACCESSION MR: AP3COO494

5/0145/63/000/001/0097/0107

AUTHOR: Ivanov, V. L. (Candidate of technical sciences)

TITLE: Toward the calculation of nozzle-blade cooling by air

SOURCE: Izv. WUZ: Mashinostroyeniye, no. 1, 1963, 97-107

TOPIC TAGS: high-temperature turbine, blade cooling

ABSTRACT: The problem of nozzle-blade cooling in high-temperature turbines is examined. Both theoretical considerations and experimental research show that nozzle blades are exposed to air cooling in all systems of rotor-blade cooling. The choice of parameters of the cooling system is based on the temperature distribution on the blade surface and on the power losses in the cooling system. The calculation of the blade temperature is carried out on the basis of averaged parameters. The temperature field of the blade is divided into four distinct regions: 1) leading edge, 2) convex side, 3) concave side, and 4) trailing edge of the convex side. Equations describing the temperature

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L 11260-63 ACCESSION NR: AP3000494 variations in each of the regions are derived, and formulas are given for determining the temperature of the cooling air, the coefficients of heat transfer from the cooling air, and local values of the wall temperatures. A differential equation is derived for the determination of the pressure drop of the cooling air in the flow past the cooled surface of the blade, and a table of values of the integral constant is given. Orig. art. has: 38 formulas, 2 tables and 6 figures. ASSOCIATION: MVTU im. N. E. Baumana SUBMITTED: 25Apr62 DATE ACQ: 21Jun63 ENCL: 00 SUB CODE: PR, AE NO REF SOV: OOL Card 2/2

IVANOV, V.L., kand.tekhn.nauk

Investigating heat exchange in a closed channel under natural convection conditions in case of a change in the state of age gregation of the heat carrier. Izv.vys.ucheb.zav.;mashinostr.no. 1:117-129 *63.

(MIRA 16:5)

l. Moskovskoya vyssheye tekhnicheskoye uchilishëlim imeni Baumana. (Heat—Transmission)

I VANOV, K.L.

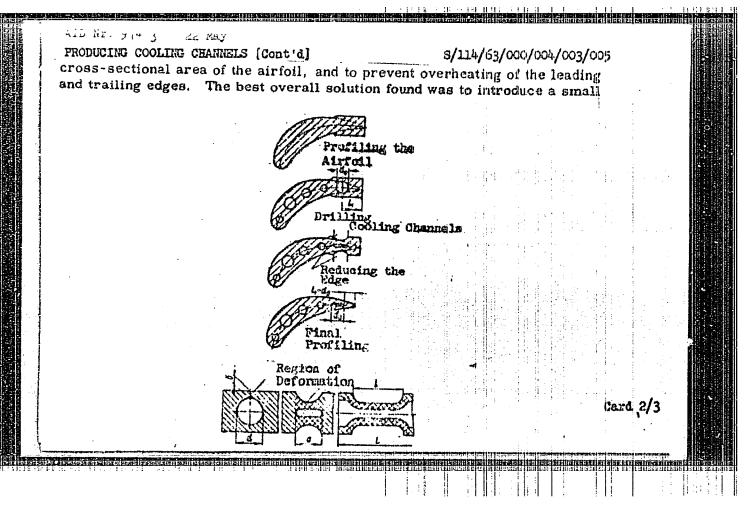
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Producing cooling Channels in Gas turbine blades (USSR)

Ivanov, V. L., A. G. Zasimov, and I. M. Stanishevskiy. Energomashino-stroyeniye, no. 4, Apr 1963, 31-34. S/114/63/000/004/003/005

The development of high-temperature gas turbines depends on the rational design of internally cooled turbine blades. Investigations to determine procedures for the manufacture of such blades have been carried out at the Research Laboratory of Turbine Construction, Moscow Higher Technical School, under the supervision of Professor V. V. Uvarov. The main problems were to reduce to a minimum the deviation of the airfoil profile from that of the uncooled blade, to assure maximal uniformity of the temperature field along the

Card 1/3



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the trailing ϵ	edge and then r	educe the channel	by means o	f punch	es or ro	llers			
[AISI 330] st	e more produc eel blades red	tive). Experiment ucing channels 3 m	s were car	ried out	on 3N	612 mrn wi	de		
with or witho	out preheating	the blade. Although	h the stren	gth of h	ot-and	cold-de			
formed blade	es was the sam	e after similar he	at treatmen	t, hot v	vorking	is reco	m-		
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IVANOV, V.L., kand. tekhn. nauk

Calculating heat transmission by a ribbed surface, Izv. vys. ucheb. zav.; mashinostr. no.9:174-183 '63.

(MIRA 17:3)

1. Moskovskoye vyssheye tekhnicheskoye uchilishche imeni Baumana.

MANUSHIN, E.A., inzh.; IYANOV, V.L., kand. tekhn. nauk

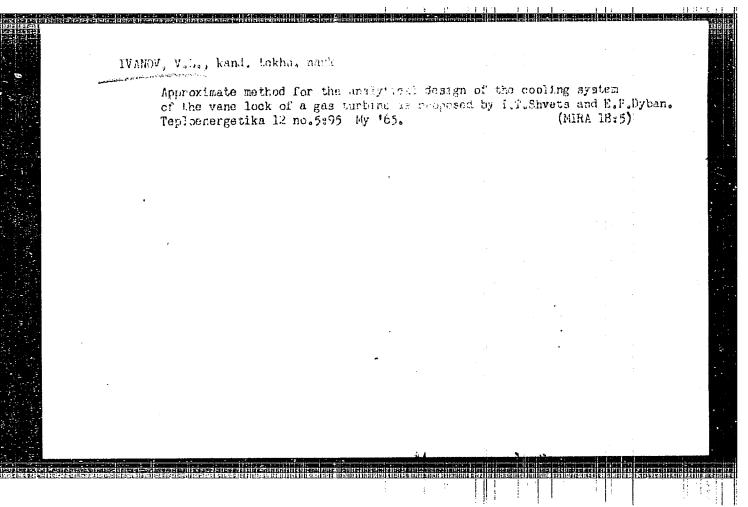
Effect of cooling on hydraulic efficiency of the blading of a high-temperature gas turbine. Izv. vys. ucheb. zav.; mashinostr. no.9:184-189 '63. (MIRA 17:3)

1. Moskovskoye vyssheye tekhnicheskoye uchilishche imeni Baumana.

ALEXSANDROV, G.N., kand. tekhm. neak; IVANOV, V.L., inxh.

Dependence of the electrical strength of long air gaps on the frequency of the oscillatory voltage. Elektrichestwo no.6:
44-49 Je'64 (MIRA 17:7)

1. Leningradskiy politekhnicheskiy institut.

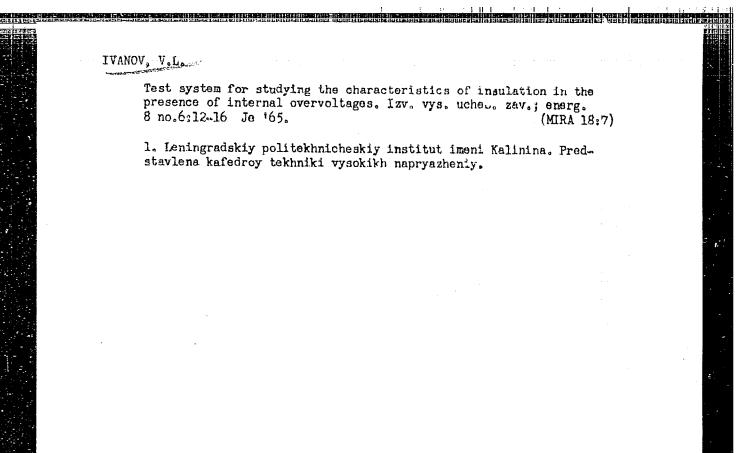


ALEKSANDROV, G.N., kand. tekhn. nauk; IVANOV, V.L., inzh.; HEDROV, V.P., inzh.

Electrical strength of an air gap between the wire of a superhigh voltage transmission line and ground in the presence of internal overvoltages. Elektrichestvo no.4:20-24 Ap '65.

(MIRA 18:5)

1. Leningradskiy politekhnicheskiy institut.



ACC NR: AP6017840	SOURCE CODE:	UR/0147/66/000	/002/0143/0	0150
UTHOR: Ivanov, V. L.; Manushin, E.	. A.; Lapin, Yu.	<u>D.</u>		50 B
RG: none		ž	nestigi	4
TTLE: Some results of an experimen	ntal investigation	of a cooled turk	ine	
OURCE: IVUZ. Aviatsionnaya tekhnik	ka, no. 2, 1966, 1	43-150		
OPIC TAGS: gas turbine, high tempe otor blade cooling	erature turbine, t	urbine cooling, r	otor blade	•
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BSTRACT: The <u>cooling</u> of a <u>high-tem</u> iquid-cooling system has been inves	mperature turbine i	otor with a natu	ral-convec	tion
rried water circulated by a high-br	ressure centrifucal	numn. For mose	urina tha	•
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ACC NR: AP7006676

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SOURCE CODE: UR/0145/66/000/010/0070/0072

AUTHOR: Ivanov, V. L. (Candidate of technical sciences, Lecturer); Lapin, Yu. D. (Candidate of technical sciences)

ORG: None

TITLE: Heat exchange under conditions of free convection in a section of a channel with localized resistance

SOURCE: IVUZ. Mushinsotroyeniye, no. 10, 1966, 70-72

TOPIC TAGS: convective heat transfer, flow analysis, hydraulic resistance, Nusselt number

ABSTRACT: The authors consider the characteristics of free convective heat exchange in a section of channel with local hydraulic drag (channel inlet). The fundamental relationship for this section in the case of turbulent flow conditions is

$$Nu^* = \frac{Q}{\lambda \Delta t_u D} - f(\zeta) (Or Pr^2)^{0.5},$$

where λ is the coefficient of thermal conductivity for the heat-exchange medium, Q is the thermal flux in the channel, Δt_{M} is the variation in the average temperature of the heat-exchange medium in the input section, D is the dismeter of the channel in the

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UDC: 621.43

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blade, Nu* is the conditional Nusselt number, $f(\zeta)$ is a function of the coefficient of local hydraulic resistance at the channel input (ζ) . It is shown that the function $f(\zeta)$ may be written as

A MANAGE A SECTION OF A SECTION

$$f(\zeta) = f_1 \left[\left(\frac{D}{d} \right)^2 \right].$$

Experimental studies on stationary models confirm this relationship. Experimental data reduced to dimensionless form are satisfactorily described by the equation

$$Nu^{\bullet} = \frac{Q}{\lambda \Delta I_{\mu} D} = A (Gr Pr^2)^{0.5},$$

Where A is a coefficient which depends on area ratio F. Experimentally determined values of this coefficient are tabulated. The article was presented for publication by Doctor of technical sciences V. V. Uvarov, Professor at the Moscow Technical College im. N. E. Bauman. Orig. art. has: 1 figure, 1 table, 2 formulas.

SUB CODE: 20/ SUBM DATE: 30Mar66/ ORIG REF: 002

Card 2/2